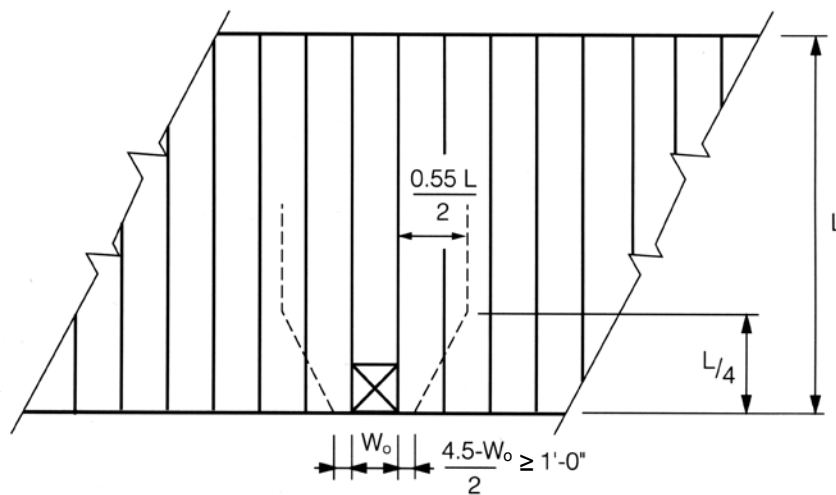


SHEAR DESIGN AT END OPENINGS

Research on load distribution has been a major part of the continuing testing program conducted by the Spancrete Manufacturers Association.



EFFECTIVE RESISTING SLAB WIDTH AT END OPENINGS

CONCLUSIONS:

1. Openings at the end of a span will cause a concentration of shear stresses due to shear and torsion at the sides of an opening.
2. The midspan region will not be affected by an end opening as long as strand development occurs after the opening and before the area of maximum moment.
3. The effective resisting section shown is recommended for shear design around end openings. The design procedure is to superimpose on the uniform loads the distributed load concentrations.

A design example is given on the reverse side.

SHEAR DESIGN AT END OPENINGS

GIVEN:

An 8" x 40" Spancrete® hollowcore system as shown.
 Self-weight = 64 psf, uniform superimposed
 dead and live loads are 10 psf and 40 psf

PROBLEM:

Select the prestress, check strand
 development, and check shear.

SOLUTION:

- From load tables, for a total superimposed load of 50 psf, select eight 5/16" dia. 250 ksi strands with 3/4" clear cover. Use 65% for initial tension and assume 20% losses, and concrete strength of 5000 psi
- Check strand development from opening

L_d required = $(f_{ps} - 2/3f_{se}) d_b = (.98 \times 250 - 2/3 \times .65 \times .8 \times 250)/5/16 = 50"$
 L available = $(\frac{25}{2} - 3)12 = 114" > 50"$ OK
- Check shear caused by the additional concentration of load from the strip of slab containing the opening.

Plank bearing = 4"

At h/2, distribution width $DW = 1 + \frac{.333}{6.25} (\frac{13.75}{2} - 1) = 1.31'$

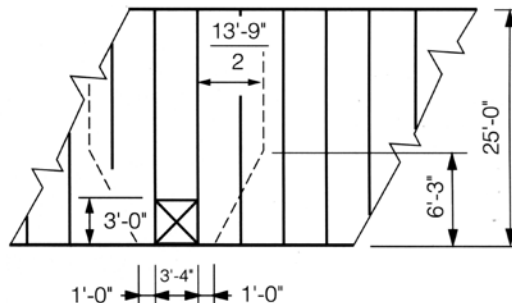
$W_u = 1.2 (10 + 64) + 1.6 (40) = 153$ psf from uniform loads

Distribute load from strip with opening and superimpose

$W_u = 153 + (\frac{153 \times 3.33}{1.31 \times 2}) = 348$ psf

Checking shear at critical points, find:

$\phi v_{cw} = 203$ psi $> v_u = 118$ psi and $\phi v_{ci} = 106$ psi $> v_u = 78$ psi. Shear check is OK.
- If inclined shear had not checked at some point in the span, calculate a new effective width at that point, determine a new distributed load, and recheck shear.



Additional information for Shear Design is provided in Research Note title, "SHEAR STRENGTH"

Note: Sample calculations are intended to illustrate the concept presented and do not represent all considerations necessary for the complete design. This research was done using 40" wire, 8" thick Standard Spancrete. However, this concept applies to all Spancrete cross sections.

EAST

Oldcastle Precast, Inc.
 South Bethlehem, NY

Oldcastle Precast, Inc.
 Manchester, NY

Conewago Precast Building
 Systems
 Hanover, PA

MIDWEST
 Spancrete, Inc.
 Green Bay, WI

Spancrete Industries, Inc.
 Waukesha, WI

Hanson Structural Precast
 Midwest, Inc.
 Maple Grove, MN

Spancrete of Illinois, Inc.
 Arlington Heights, IL

WEST

Hanson Structural Precast
 Pacific, Inc.
 Inwindale, CA

KIE-CON
 Div. of Kiewitt Pacific Co.
 Antioch, CA

Owell Precast
 Sandy, UT

SOUTHWEST
 Manco Structures, Ltd.
 Schertz, TX

SOUTH

Cement Industries, Inc.
 Fort Myers, FL

Florida Precast Industries, Inc.
 Sebring, FL

MC Precast, Inc.
 Atlanta, GA

CANADA
 Burnco Concrete Products Ltd.
 Calgary, Canada

EGYPT
 Samcrete Egypt
 Ahram, Giza

MEXICO

ITISA
 Mexico City, Mexico

Spancrete Noreste
 Monterrey, Mexico

TURKEY
 Yapi-Merkezi
 Camlica-Istanbul, Turkey

CARIBBEAN
 Preconco Limited
 Barbados, West Indies

Spancrete Caribbean, Ltd.
 Trinidad, West Indies

UAE
 Hi-Tech Concrete Products, LLC
 Abu Dhabi, UAE

MACHINE MANUFACTURER

Spancrete Machinery
 Corporation
 Waukesha, WI

Spancrete is also manufactured in

Armenia	Denmark	Russia
Australia	Guatemala	South Korea
Belgium	Hungary	Spain
Brazil	Ireland	Switzerland
China	Israel	
Croatia	Japan	